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ļ	2. ECN Category (mari	k one)	3. Originator's Name,	Organization, MSIN, and To	elephone No.		4. Date	
Ì	Supplemental Direct Revision		G. F. Willian	nson, 82920, R4-0	03, 3-5922		7-31-90	
	Change ECN		5 Project Title/No./Wo W-125 and	rk Order No. J 864	ح- 6. Bidg.	'Sys./Fac. No.	7. Impact Level	
1	Temporary Supersedure		B-714 Grout (Disposal Faciliti	ies 218	-E-16	2	
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	S. R. Briggs R. D. Clagho O. A. Halvor G. W. Jackso J. R. McGee R. L. Moxin D. R. Nunama D. B. Powell	orn son on	R4-02 D. R3-09 T. R4-01 A. S1-54 J. S4-43 G. S5-04 M. R4-03 J.	J. Powell R. Pratt W. Staehr R. Tedeschi E. Van Beek F. Williamson W. Cline S. Hill	R4-03 T1-30 R3-27 R4-02 R3-27 R4-01 R4-02	OFFIC:	AL RELEASE CONTROL OCT 29 1990	
	R. K. Sanan			A. Karnesky A. Voogd	R4-03 R4-03		A-7900-013 (11/8	

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ENGINEERING CHANGE NOTICE								Page 2 of	1. ECN (use no. from pg. 1)		
15. Design Verification 16. Cost Impact				ENGINEERING			CONSTRUCTION		17. Schedule Impact (days)		: (days)
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18 Change Impact Review: Indicate the related documents (other than t							docume	nts identified on Si	de 1) that will	be affe	cted by
the change described in Block 12. Enter th SDD/DD Functional Design Criteria Operating Specification Criticality Specification Conceptual Design Report Equipment Spec Const. Spec Procurement Spec. Vendor Information OM Manual FSAR/SAR Safety Equipment List Radiation Work Permit Environmental Impact Statement Environmental Report Environmental Permit 19 Other Affected Documents: (NOTE: Document Number/Revision V-B714C2-003 WHC-SD-WM-SAR-042				Seismic/Stress Analysis Stress/Design Report Interface Control Drawing Calibration Procedure Installation Procedure Maintenance Procedure Engineering Procedure Operating Instruction Operating Procedure Operational Safety Requirement IEFD Drawing Cell Arrangement Drawing Essential Material Specification Fac, Proc. Samp. Schedule Inspection Plan Inventory Adjustment Request Is listed below will not be revised by the documents listed below Document Number/Revision				Spares Multiple Unit Listing Test Procedures/Specification Component Index ASME Coded Item Human Factor Consideration Computer Software Electric Circuit Schedule ICRS Procedure Process Control Manual/Plan Process Flow Chart Purchase Requisition			<u> </u>
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	OPERATIONS AND ENGINEERING Cog./Project Engineer						ENGINE	<u>ER</u>			
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1. Add a section 2.2.14

<u>Diffusion Cocoon Requirements</u>

The function of the cocoon is to control the release of radionuclides and chemicals from the grouted waste disposal system to the environment. The cocoon functions in two important ways to provide this additional isolation and environmental protection.

- . The long-term release of radionuclides and chemical constituents is delayed by decreasing the diffusivity of the barrier system. The function of the asphalt barrier is to provide an effective ionic diffusivity of at least 1 X E^{-10} cm²/sec, (reference 8).
- The asphalt concrete cocoon keeps water from entering the waste form. The high salt liquid tank waste is combined with a tailored blend of cementitious bulk solids to form a grout slurry which is placed in the vault for curing and disposal as a solid waste form. After the initial heat of hydration is completed, a longer term radiolytic heating will take place such that the grouted waste will be at an elevated temperature compared to the surrounding soil for hundreds of years. Eventually, the moisture in the soil column in the form of water vapor will be attracted to the high salt grouted waste once isothermal conditions are reached. The cocoon will serve as a water vapor barrier with vapor diffusivity of less than 2.9 X 10⁻⁵ cm²/sec to prevent the return of moisture to the grouted waste (reference 8). This prevents the saturation of the grout and eventual release of contaminants due to "dripping" through the bottom of the disposal system.

2. Add a section 2.2.15

The cocoon is also to be designed to perform its intended function for a long time period. The disposal system is to be designed so that there is a reasonable expectation that performance of the undisturbed system does not exceed the dose limits outlined in DOE Order 5820.2A and Draft DOE-RL 5820.2A for 1,000 years after disposal.

Draft DOE-RL 5820.2A defines ALARA for long term protection. Reasonable effort shall be made to design disposal systems such that potential exposures are ALARA for all times up to the year of maximum exposure.

3. Add a section 2.2.16

Based on significant development work and performance assessments provided by others (WHC and PNL), the following design features and criteria are expected to satisfy the functional and performance requirements for the cocoon. Use of an asphalt cocoon placed around all exterior surfaces of the vault and lower liner will provide the required degree of waste isolation from the soil column and ultimately the groundwater and fulfill the ALARA requirements for an estimated 10,000 year time frame.

- Asphalt composition shall be Grade AR-6000 and provided in a mix of 7.5 ± 0.5 weight percent asphalt.
- Aggregate shall consist of crushed stone or gravel with a size distribution as shown in Table 1.
- Aggregate shall be coated with an antistripping agent, 3 \pm 0.5 weight percent lime, prior to asphalt addition.
- The asphalt mixture shall pass modified Texas Boil and Lottman (WSDOT 718) stripping tests using distilled water and a NaOH solution of pH 12.
- The asphalt mixture shall have a minimum compressive strength of 370 PSI at 90°C by ASTM D 1074-83 (or latest equivalent).
- For project W-125 the thickness of the cocoon shall be a minimum of 40 in. around all exterior surfaces of the vault and leachate collection system.
- Project B-714 shall have a minimum asphalt cocoon thickness of 18 in. under the vault catch basin, (reference 8) and shall be a minimum of 36 in. thick from the catchbasin bottom to the upper lip of the catchbasin. Asphalt cocoon thickness above the upper lip of the catchbasin shall be a minimum of 40 in. on all other exterior surfaces of the vault and leachate collection system.
- The asphalt mixture shall be compacted to provide uniform and continuous coverage around the vault system with a maximum of 4 percent voids. The permeability tests on compacted specimens are to be in general accordance with ASTM D3637.

Justification:

To provide functional criteria for a cocoon (barrier) to meet long-term performance requirements described in the Grouted Double-Shell Tank Waste Performance Assessment (reference 8).

Page 45 of 87 140503

TABLE 1 (Reference 6)

Grading in accordance with ASTM C 136.

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. Amounts finer than each laboratory sieve (square-openings), weight percent.

Nominal Square Opening <u>Sieve Size</u>	Aggregate <u>Percent</u>			
5/8 in.	100			
1/2 in.	92 to 100			
3/8 in.	85 to 95			
No. 4	65 to 75			
No. 16	35 to 41			
No. 30	25 to 31			
No. 50	14 to 20			
No. 200	3.5 to 7.5			

- Deleterious materials: Particles of specific gravity less than 1.95, maximum 1% by weight.
- Limits for fractured faces by percent weight: Minimum of 2 fractured faces on 85% and at least 1 fractured on 90% of material retained on No. 10 and above sieves.

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4. Change existing section 2.7 to 2.8 and add a section:

2.7 GAS VENTING REQUIREMENTS:

Two small gas vents shall be provided from the lip of the catch basin through the cocoon to the soil column. The vents shall have a nominal inside diameter of approximately 0.1 in. to prevent pressurization and allow any accumulation of hydrogen due to radiolytic decay to escape from the waste disposal system to the soil column (reference 5). Other functional requirements include:

- Minimum design life 250 years
- Nominal diameter .1 Inch (I.D.)
- Minimum vent opening distance from vault barrier: 4-feet
- Minimum distance from any other potential void or area that would tend to concentrate the gas shall be 4-feet
- Ignition sources are to be eliminated from the vault catch basin and the soil, including the leachate sump.
- The vent should be approximately 1 inch in diameter at the soil and filled with pea gravel with a screen to keep the gravel in place.
- The hole in the diffusion break shall not be larger than .5 inch in diameter.

The location of the vents should be at the end of the vault opposite the leachate collection tank (one in each corner) and just above the lip of the concrete catch basin. The compressive strength of the vent tube shall be adequate to allow compaction of the asphalt barrier around the tube without collapsing the tube.

The ends of the tube should be connected to a nominal I inch diameter pipe with an abrupt entry of the tube into the pipe and a screen just beyond the exit of the tube to prevent clogging of the tube. The pipe section should be filled with appropriate material before installation to prevent clogging of the pipe and to reduce the pressure drop in venting to the soil.

The gas vent placement should be designed to prevent hydrogen gas build-up in any area that would tend to concentrate the gas, such as the diffusion barrier.

Design to Safety Class 2, as defined by WHC procedures. The two vents are redundant in that only one is required for operation.

Maximum pressure to be seen by the vent piping is less than 50 PSI.

7 Page 8 of 8 140503

Justification:

Over a period of time, radiolytic hydrogen can be produced from the grout waste as hydrogen gas. To prevent the gas from slowly building up and pressurizing the grout vault it is necessary to install small vents through the solid diffusion break. Gas will vent through this small exit with only small back pressures. The impact on the performance assessment of water vapor diffusing back through the vent is negligible. After 250 years the rate of gas generation will be small enough so that if the vent closes, the hydrogen can be released by diffusion through the solid asphalt diffusion barrier that surrounds the grout vault.

Add to Section 4.0:

DOE-RL 5820.2A (Draft), "Radioactive Waste Management, July 1990

Add to section 6.0:

- 5. HGTP-90-02-01, "GAS GENERATION AND RELEASE FROM DOUBLE-SHELL SLURRY FEED (DSSF) GROUT VAULTS", G. A. WHYATT, December 1989 Draft.
- Letter, W. J. Powell to Distribution, "Asphalt Diffusion Break and Barrier Material Properties," June 28, 1990.
- 7. SD-WM-CR-029, Rev. 2, "Design Criteria for the Grout Disposal Vault Ventilation System," April 30, 1990.
- 8. PNL Report, G. A. Whyatt, et. al., "Performance Assessment of Grouted Double-Shell Tank Waste Disposal at Hanford," June 1990 Draft.